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Reduced polynomial invariant integrity basis for in-plane magneto-mechanical loading.

J. Taurines*, B. Kolev, R. Desmorat, O. Hubert

Université Paris-Saclay, CentraleSupélec, ENS Paris-Saclay, CNRS, LMPS laboratoire de Mécanique, 4 avenue des sciences, Gif-sur-Yvette, 91190, France

Abstract

The description of the behavior of a material subjected to multi-physics loadings requires the formulation of constitutive laws that usually derive from Gibbs free energies, using invariant quantities depending on the considered physics and material symmetries. On the other hand, most of crystalline materials can be described by their crystalline texture and the associated preferred directions of strong crystalline symmetry (the so-called *fibers*). Moreover, among the materials produced industrially, many are manufactured in the form of sheets or of thin layers. This article has for object the study of the magneto-mechanical coupling which is a function of the stress $\boldsymbol{\sigma}$ and the magnetization \mathbf{M} . We consider a material with cubic symmetry whose texture can be described by one of three fibers denoted as θ , γ or α' , and which is thin enough so that both the stress and the magnetization can be considered as in-plane quantities. We propose an algorithm able to derive linear relations between the 30 cubic invariants I_k of a minimal integrity basis describing a magneto-elastic problem, when they are restricted to in-plane loading conditions and for different fiber orientations. The algorithm/program output is a reduced list of invariants of cardinal 7 for the $\{100\}$ -oriented θ fiber, of cardinal 15 for the $\{110\}$ -oriented α' fiber and of cardinal 8 for the $\{111\}$ -oriented γ fiber. This reduction (compared to initial cardinal 30) can be of great help for the formulation of low-parameter macroscopic magneto-mechanical models.

Keywords: Invariants, Integrity basis, Strong coupling, Thin structures, Magnetostriction

*Corresponding author

Email address: julien.taurines@ens-paris-saclay.fr (J. Taurines)

1. Introduction

Since the discovery of the crystalline nature of metals, and of the anisotropic nature of the associated behaviors, metallurgists have sought to improve thermomechanical treatments in order to develop the most favorable crystallographic textures. Research is carried out, in particular, on magnetic materials [6, 23]. In this regard, we can cite the well-known *Goss* texture for 3%silicon-iron alloys [29] used as vehicles of the magnetic flux in high power transformers: the magnetic permeability in the rolling direction is greatly improved comparing to the magnetic permeability of an isotropic 3%silicon-iron polycrystal; the coercive field is considerably reduced, leading to a drastic decrease of energy losses per magnetization cycle. References [26, 43, 34] thus report recent developments in this field. On the other hand, cold rolled and annealed FeNi alloys are known to be able to develop a so-called *cube* texture during recrystallization [1, 44], meaning that the crystallographic frame coincides with the sheet frame: this texture leads to a high magnetic permeability in both the rolling and transversal (to the rolling) directions. For their part, magnetic shape memory alloys (MSMA) are generally produced as single crystalline bulk materials since polycrystals exhibit lower magneto-mechanical and fatigue performances. Recent works show the possibility of producing hypertextured polycrystalline Ni-Mn-Ga MSMA and possibly in the form of thin layers, opening a wide new range of applications [28]. Conversely, the crystallographic texture can be high and uncontrolled. This is frequently observed for very thin magnetic materials used in high frequency electronic systems [5, 47, 22] (the small thickness allows for a better homogeneity of the electromagnetic fields through the thickness at very high frequency, typically GHz). The textures encountered may vary but generally follow epitaxy rules (depending on the sublayer orientation): the direction normal to the layer is frequently a direction of strong crystalline symmetry. Finally, the increasing miniaturization of electronic systems is pushing for the use of small size –therefore thin– magnetic components. We thus observe an increasing scale confusion between component and crystals, making behaviors very sensitive to surface effects [25]. Moreover, just like a magnetic material magnetizes under the effect of a magnetic field, it deforms. This deformation, called magnetostriction, is the first manifestation of the magneto-elastic coupling [18]. The inverse magneto-elastic coupling is the effect of a mechanical stress on the magnetic behavior (the Villari effect) [4, 7]. Some mate-

materials such as 3% silicon-iron or 27% cobalt-iron alloys develop such a sensitivity to mechanical loading that a *non-monotony* appears : magnetic permeability increases at low stress level (in uniaxial condition), then it decreases with increasing stress at higher stress level. Some few explanations that have been proposed (microplasticity, stress field heterogeneity) are not tenable because the non-monotony is reversible and the stress levels are insufficient to lead to a magnetization rotation. The magnetostriction measurements also confirms that it is a fully coupled magnetoelastic phenomenon that cannot be addressed by classic magnetoelasticity. The introduction of a second-order (quadratic both in $\boldsymbol{\sigma}$ and in \boldsymbol{M}) magneto-elastic coupling term in the expression of the Gibbs free energy density makes it possible to account for this effect (defined as the morphic effect in [17]): simulations and model-experiment comparisons have been proposed in [24] using a second-order isotropic approximation. The isotropic approximation is however reductive given the cubic symmetry of the medium. The development of a cubic second order term however requires the use of a 6th order tensor. Its construction and handling are difficult. The approach by *Invariant Theory* and the use of a *minimal* integrity basis (see [32, 13]) are the core of a recent article dealing with magneto-elastic coupling in cubic media [42]. It allows for a rigorous construction of Gibbs free energy density at any order without missing any term.

However, this integrity basis has a large cardinal ($= 30$), which can make the identification process very cumbersome, when higher order terms are involved. Indeed, during tests carried out on thin gauge samples, quantities like strain and magnetic field are not measurable through the thickness and the full identification of the material constants is not possible. It joins the idea of *mechanically accessible directions for measurements* described in [15].

In this paper, we consider thin textured sheets for which the integrity basis given in [42] can be reduced when only in-plane magneto-mechanical loadings are considered. Indeed, the magnetization of the material is assumed to remain in the sheet plane due to the strong demagnetizing fields created by any emergent magnetization [23]. This boundary condition is completed by the usual plane stress assumption. Finally, small deformation hypothesis is used in all formulations.

The paper is organized as follows. In [section 2](#), we present the main concepts related to the definition of a crystallographic texture for materials with cubic symmetry. In [section 3](#),

we introduce cubic magneto-elasticity energy densities and the fundamental 30 invariants I_k obtained in [42] which are necessary to formulate them. The mathematical formalism used to describe in-plane loadings and reduce the number of fundamental invariants for these loadings is introduced in section 4. The results for the three main material fibers are provided in details in section 5. Finally, an algorithm and its implementation in *Macaulay2* to obtain relations between the evaluated invariants I_k for some given crystallographic textures is proposed in Appendix Appendix A. The output is a minimal list of polynomial invariants that allows for the most general expression of Gibbs free energy density to be formulated for a large set of crystallographic textures.

2. Texture and orientation data function of crystalline materials

The crystallographic texture is a simplified description of how the individual crystallites that make up the material are distributed. In materials science, Euler angles are used to describe a single crystal orientation relative to the axes of the sample (as the reference orthonormal frame). The following denomination is usually employed and illustrated in Figure 1: $\mathbf{r} = RD$ for Rolling Direction, $\mathbf{t} = TD$ for Transversal Direction and $\mathbf{n} = ND$ for Normal Direction indicate the reference orthonormal frame. Such denominations are obviously borrowed from sheets metallurgy and rolling process.

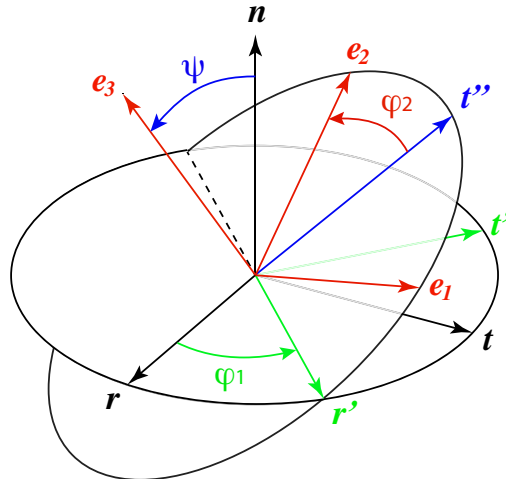


Figure 1: Illustration of reference $(\mathbf{r}, \mathbf{t}, \mathbf{n}) = (RD, TD, ND)$ and rotated $(\mathbf{e}_1, \mathbf{e}_2, \mathbf{e}_3)$ frames using $(\varphi_1, \psi, \varphi_2)$ Euler angles and Bunge rotation rules.

The three angles defining the orientation of crystal axes relative to the reference frame are noted $(\varphi_1, \psi, \varphi_2)$ using Bunge representation:

- φ_1 corresponds to a first rotation operation around ND axis; the new coordinate system is named $(\mathbf{r}', \mathbf{t}', \mathbf{n})$.
- ψ corresponds to a second rotation operation around \mathbf{r}' axis; the new coordinate system is named $(\mathbf{r}', \mathbf{t}'', \mathbf{e}_3)$.
- φ_2 corresponds to a third and last rotation operation around \mathbf{e}_3 axis; the new frame is denoted $(\mathbf{e}_1, \mathbf{e}_2, \mathbf{e}_3)$.

Associating the cubic crystallographic frame $([100] [010] [001])$ to the orthonormal frame $(\mathbf{e}_1, \mathbf{e}_2, \mathbf{e}_3)$, it is possible to observe some connection between a crystallographic axis $[uvw]$ and the principal axes of the reference frame. We thus usually designate by the following Miller indices combination

$$\{hkl\} \langle uvw \rangle$$

a situation where $\{hkl\}$ corresponds to ND (for cubic symmetry, h, k and l also indicate the components of the vector normal to the sheet plane) and where $\langle uvw \rangle$ corresponds to RD .

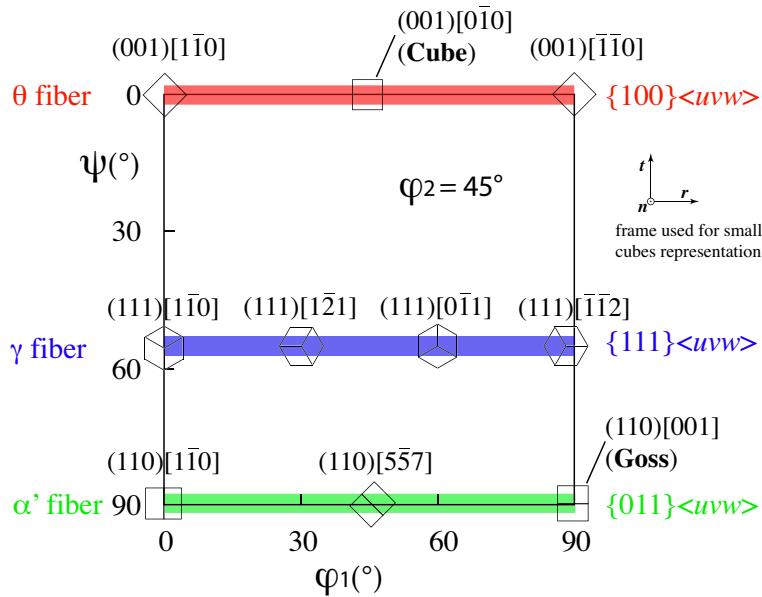


Figure 2: Cut of Euler space for $\varphi_2 = 45^\circ$ and highlighting of some major texture components.

Some remarkable directions do obviously correspond to a given set of Euler angles. It is thus possible to place some of these remarkable directions in a (φ_1, ψ) plane for a fixed φ_2 . Figure 2 illustrates a cut of the Euler space for $\varphi_2 = 45^\circ$, highlighting some remarkable orientations. The three main situations colored in red, green and blue are:

- θ fiber: $\{100\}\langle uvw \rangle$ - the normal plane corresponding to a cube face;
- α' fiber: $\{110\}\langle uvw \rangle$ - the normal plane corresponding to a cube diagonal plane;
- γ fiber: $\{111\}\langle uvw \rangle$ - the normal direction corresponding to a cube trisectrix.

When specific planes and directions are considered (and not direction and plane families), parentheses and brackets are used. We highlight the following *classical* textures:

- Cube texture, belonging to θ fiber: $(001)[0\bar{1}0]$;
- Goss texture, belonging to α' fiber: $(110)[001]$.

Of course, most materials do not present a single $\{hkl\}\langle uvw \rangle$ orientation but a set of orientations, corresponding to a set of Euler angles and defining the orientation data function (ODF). A material is denoted as *textured* when this distribution is tightened on one or more particular directions. Otherwise, it is a non-textured material. Magnetic materials obtained by rolling process or deposit thus often present pronounced textures that can be found in the above list ¹. Some others may be described by a combination of these textures [31, 10]. A texture can thus represent, beyond a simple assembly of crystals, the material itself, thereby allowing for a macroscopic modeling, ignoring its multiscale nature. Within the framework of the development of magnetoelastic constitutive laws of any order, taking into account the existence of a texture can lead to significant simplifications. We focus our efforts on the three main fibers listed above.

¹Other textures are referenced in literature -so called *brass* texture, *copper* texture, α fiber, ϵ fiber and so on - but they do not exhibit a single crystallographic direction perpendicular to the sheet plane.

3. Cubic magneto-elasticity

There are two main manifestations of magnetoelastic coupling in magnetic materials: the magnetostriction and the variation of the magnetization under stress. The modeling which is proposed in the literature is generally based either on constitutive tensors (of order 3 and higher [24, 30]) or on well chosen invariants [19, 9]. Such a modeling can also be carried out at different scales from microscopic to macroscopic. At the crystal scale, magnetization is associated with the cubic (octahedral) symmetry group \mathbb{O} which is defined by

$$\mathbb{O} = \{g \in O(3); g\mathbf{e}_i = \pm\mathbf{e}_j\},$$

where (\mathbf{e}_i) is the canonical orthonormal basis of \mathbb{R}^3 and $O(3)$ is the orthogonal group. This group is of order 48 : it contains 24 rotations and 24 orientation-reversing isometries leaving the cube invariant [45]. The stress tensor $\boldsymbol{\sigma}$ and the magnetization pseudo-vector \mathbf{m} (with $\|\mathbf{m}\| = m_s$ the saturation magnetization) are almost homogeneous at this scale. The macroscopic behavior, *i.e.*, at the representative volume element (RVE) scale of volume V , is obtained by an homogenization process [11]. The macroscopic magnetization is, for example, given by

$$\mathbf{M} = \langle \mathbf{m} \rangle = \frac{1}{V} \int_V \mathbf{m} dv. \quad (3.1)$$

A direct description of the macroscopic behavior by using a well chosen expression of the Gibbs free energy density is an alternative approach. For instance, isotropic energy densities have been proposed in [38, 36], transversely isotropic ones in [8] and orthotropic ones in [35]. Cubic invariants of the pair $(\mathbf{m}, \boldsymbol{\sigma})$ [39, 42], fully relevant at the magnetic domains scale, may also be relevant at the macroscopic scale, by considering the macroscopic magnetization \mathbf{M} in place of the local magnetization \mathbf{m} , *if cubic symmetry applies at the macroscopic scale*. As extensively explained in the introduction of this paper, this situation is encountered in single crystals, or when the material, consisting of an assembly of cubic crystals, is highly textured.

Classical Invariant Theory [41, 33] is a robust and efficient tool which helps to formulate Gibbs energy densities that respect the material symmetry, the key points of this theory being

1. the choice of the relevant group G for the material symmetry/physics [27, 3],

2. the determination of an integrity basis $\{I_k\}$ or, more generally, of a functional basis [46].

Therefore, each ~~magneto-elasticity~~ Gibbs free energy density which is G -invariant can be expressed as

$$\Psi = \Psi(I_k). \quad (3.2)$$

In the following, we consider a cubic microstructure, *i.e.*, a microstructure which is invariant by the octahedral symmetry group $G = \mathbb{O}$, and where the set $\{I_k\}$ is the integrity basis for polynomial cubic invariants in \mathbf{M} and $\boldsymbol{\sigma}$ provided in Table 1.

$\deg(\mathbf{M})$	$\deg(\boldsymbol{\sigma})$	Formula	Tri-graded notation
0	1	$\text{tr } \boldsymbol{\sigma}$	–
0	2	$\boldsymbol{\sigma}^{\bar{d}} : \boldsymbol{\sigma}^{\bar{d}}$	I_{002}
0	2	$\boldsymbol{\sigma}^d : \boldsymbol{\sigma}^d$	I_{020}
0	3	$\text{tr}(\boldsymbol{\sigma}^{\bar{d}3})$	I_{003}
0	3	$\boldsymbol{\sigma}^{\bar{d}2} : \boldsymbol{\sigma}^d$	I_{012}
0	3	$\text{tr}(\boldsymbol{\sigma}^{d3})$	I_{030}
0	4	$(\boldsymbol{\sigma}^{\bar{d}2})^{\bar{d}} : (\boldsymbol{\sigma}^{\bar{d}2})^{\bar{d}}$	I_{004}
0	4	$\text{tr}(\boldsymbol{\sigma}^{\bar{d}}\boldsymbol{\sigma}^d\boldsymbol{\sigma}^{\bar{d}}\boldsymbol{\sigma}^d)$	I_{022}
0	5	$(\boldsymbol{\sigma}^{\bar{d}}(\boldsymbol{\sigma}^{\bar{d}2})^{\bar{d}}\boldsymbol{\sigma}^{\bar{d}}) : \boldsymbol{\sigma}^d$	I_{014}
2	0	$\ \mathbf{M}\ ^2$	I_{200}
2	1	$(\mathbf{M} \otimes \mathbf{M})^{\bar{d}} : \boldsymbol{\sigma}^{\bar{d}}$	I_{201}
2	1	$(\mathbf{M} \otimes \mathbf{M})^d : \boldsymbol{\sigma}^d$	I_{210}
2	2	$(\mathbf{M} \otimes \mathbf{M})^d : \boldsymbol{\sigma}^{\bar{d}2}$	I_{202}^a
2	2	$(\mathbf{M} \otimes \mathbf{M})^{\bar{d}} : \boldsymbol{\sigma}^{\bar{d}2}$	I_{202}^b
2	2	$(\mathbf{M} \otimes \mathbf{M})^{\bar{d}} : (\boldsymbol{\sigma}^{\bar{d}}\boldsymbol{\sigma}^d)$	I_{211}
2	2	$(\mathbf{M} \otimes \mathbf{M})^d : \boldsymbol{\sigma}^{d2}$	I_{220}
2	3	$(\mathbf{M} \otimes \mathbf{M})^{\bar{d}} : ((\boldsymbol{\sigma}^{\bar{d}2})^{\bar{d}}\boldsymbol{\sigma}^{\bar{d}})$	I_{203}
2	3	$(\mathbf{M} \otimes \mathbf{M})^d : ((\boldsymbol{\sigma}^{\bar{d}2})^d\boldsymbol{\sigma}^d)$	I_{212}^a
2	3	$(\mathbf{M} \otimes \mathbf{M})^{\bar{d}} : ((\boldsymbol{\sigma}^{\bar{d}2})^{\bar{d}}\boldsymbol{\sigma}^d)$	I_{212}^b
2	3	$(\mathbf{M} \otimes \mathbf{M})^{\bar{d}} : (\boldsymbol{\sigma}^d\boldsymbol{\sigma}^{\bar{d}}\boldsymbol{\sigma}^d)$	I_{221}
2	4	$(\mathbf{M} \otimes \mathbf{M})^d : (\boldsymbol{\sigma}^{\bar{d}}(\boldsymbol{\sigma}^{\bar{d}2})^{\bar{d}}\boldsymbol{\sigma}^{\bar{d}})$	I_{204}
2	4	$(\mathbf{M} \otimes \mathbf{M})^{\bar{d}} : ((\boldsymbol{\sigma}^{\bar{d}2})^d\boldsymbol{\sigma}^{\bar{d}}\boldsymbol{\sigma}^d)$	I_{213}
2	4	$(\mathbf{M} \otimes \mathbf{M})^{\bar{d}} : (\boldsymbol{\sigma}^d(\boldsymbol{\sigma}^{\bar{d}2})^{\bar{d}}\boldsymbol{\sigma}^d)$	I_{222}
4	0	$(\mathbf{M} \otimes \mathbf{M})^{\bar{d}} : (\mathbf{M} \otimes \mathbf{M})^{\bar{d}}$	I_{400}
4	1	$(\mathbf{M} \otimes \mathbf{M})^{\bar{d}2} : \boldsymbol{\sigma}^{\bar{d}}$	I_{401}
4	1	$(\mathbf{M} \otimes \mathbf{M})^{\bar{d}2} : \boldsymbol{\sigma}^d$	I_{410}
4	2	$(\mathbf{M} \otimes \mathbf{M})^{\bar{d}2} : (\boldsymbol{\sigma}^{\bar{d}2})^{\bar{d}}$	I_{402}
4	2	$(\mathbf{M} \otimes \mathbf{M})^{\bar{d}2} : (\boldsymbol{\sigma}^d\boldsymbol{\sigma}^{\bar{d}})$	I_{411}
6	0	$\text{tr}((\mathbf{M} \otimes \mathbf{M})^{\bar{d}3})$	I_{600}
6	1	$\text{tr}((\mathbf{M} \otimes \mathbf{M})^d(\mathbf{M} \otimes \mathbf{M})^{\bar{d}}(\mathbf{M} \otimes \mathbf{M})^d\boldsymbol{\sigma}^{\bar{d}})$	I_{601}

Table 1: A minimal integrity basis [42] of \mathbb{O} -invariants for $(\mathbf{M}, \boldsymbol{\sigma})$.

A minimal integrity basis of 30 polynomials for cubic invariant polynomials in the pair $(\mathbf{M}, \boldsymbol{\sigma})$ has been obtained first by Smith, Smith and Rivlin in [39], and expressed in the components M_i and σ_{ij} of \mathbf{M} and $\boldsymbol{\sigma}$. Recently [42, Theorem 2.10 and Remark 2.11], we have proposed an alternative minimal integrity basis of invariants expressed using intrinsic tensorial expressions, rather than components. They are provided in Table 1. To obtain these invariants, the following decomposition of the stress tensor, which was introduced in [2] for cubic symmetry,

$$\boldsymbol{\sigma} = \boldsymbol{\sigma}^d + \boldsymbol{\sigma}^{\bar{d}} + \frac{1}{3}(\text{tr } \boldsymbol{\sigma})\mathbf{1},$$

has been used. In the canonical cubic basis $(\mathbf{e}_1, \mathbf{e}_2, \mathbf{e}_3)$,

$$\boldsymbol{\sigma}^{\bar{d}} = \begin{pmatrix} 0 & \sigma_{12} & \sigma_{13} \\ \sigma_{12} & 0 & \sigma_{23} \\ \sigma_{13} & \sigma_{23} & 0 \end{pmatrix}, \quad \boldsymbol{\sigma}^d = \begin{pmatrix} \sigma'_{11} & 0 & 0 \\ 0 & \sigma'_{22} & 0 \\ 0 & 0 & \sigma'_{33} \end{pmatrix}.$$

This decomposition is stable under the action of the octahedral group \mathbb{O} . In particular, for cubic materials, the deviatoric stress tensor $\boldsymbol{\sigma}' = \boldsymbol{\sigma} - \frac{1}{3}(\text{tr } \boldsymbol{\sigma})\mathbf{1}$ splits into

$$\boldsymbol{\sigma}' = \boldsymbol{\sigma}^d + \boldsymbol{\sigma}^{\bar{d}}.$$

Remark 3.1. The introduction of the following two fourth order tensors $\mathbf{P}_{\mathbb{O}}^{\bar{d}}$ and $\mathbf{P}_{\mathbb{O}}^d = \mathbf{J} - \mathbf{P}_{\mathbb{O}}^{\bar{d}}$, where

$$\mathbf{P}_{\mathbb{O}}^{\bar{d}} := \frac{1}{2} \sum_{i < j} \mathbf{e}_{ij} \otimes \mathbf{e}_{ij}, \quad \mathbf{e}_{ij} := \mathbf{e}_i \otimes \mathbf{e}_j + \mathbf{e}_j \otimes \mathbf{e}_i \quad (i \neq j).$$

and $\mathbf{J} = \mathbf{I} - \frac{1}{3}\mathbf{1} \otimes \mathbf{1}$ is the deviatoric projector, removes the dependency of this decomposition to the canonical basis (\mathbf{e}_i) . Indeed, $\mathbf{P}_{\mathbb{O}}^{\bar{d}}$ and $\mathbf{P}_{\mathbb{O}}^d$ correspond to the two orthogonal projectors of $\boldsymbol{\sigma}$ onto the \mathbb{O} -irreducible components $\boldsymbol{\sigma}^{\bar{d}}$ and $\boldsymbol{\sigma}^d$ [37, 16] in any orthonormal frame:

$$\begin{cases} \boldsymbol{\sigma}^d := \mathbf{P}_{\mathbb{O}}^d : \boldsymbol{\sigma} \\ \boldsymbol{\sigma}^{\bar{d}} := \mathbf{P}_{\mathbb{O}}^{\bar{d}} : \boldsymbol{\sigma} \end{cases}$$

This result is axis (\mathbf{e}_i) independent.

4. In-plane stress and magnetization for plates with strong crystallographic textures

General three-dimensional magneto-elasticity laws have been proposed in [42] for alloys composed of cubic symmetry crystals. Due to the quite high (= 30) cardinal of the minimal integrity basis $\{I_k\}$, recalled in Table 1, a large number of material parameters —quantified for polynomial energy densities in Table 2— has been introduced.

deg($\boldsymbol{\sigma}$) \diagdown	0	1	2	3	4	5	6	7	8	9	10
deg(\mathbf{m})											
0	1	1	3	6	11	18	32	48	75	111	160
2	1	3	9	20	42	78	138	228	363	553	819
4	2	6	19	44	95	180	323	540	867	1330	1980
6	3	10	32	78	168	324	585	984	1584	2442	3640
8	4	15	49	120	263	510	963	1560	2517	3885	5802
10	5	21	69	172	378	738	1338	2268	3663	5663	8463

Table 2: Number of material parameters [42] for polynomial energy densities (with $\|\mathbf{M}\| \neq 0$) with given bi-degree in $(\mathbf{M}, \boldsymbol{\sigma})$.

The constitutive laws linking strain $\boldsymbol{\epsilon}$ and magnetization \mathbf{M} to stress $\boldsymbol{\sigma}$ and magnetic field \mathbf{H} derive from the Gibbs free energy density Ψ :

$$\boldsymbol{\epsilon} = -\frac{\partial \Psi}{\partial \boldsymbol{\sigma}}, \quad \mathbf{H} = \frac{1}{\mu_0} \frac{\partial \Psi}{\partial \mathbf{M}}. \quad (4.1)$$

These laws can of course be evaluated for any loading, including 3D loading. However, the question of the invariants truly involved arises in a context of material constants identification. As an illustrative example, let us consider a material whose behavior is ruled by a free energy density Ψ function of 3 invariants I_1, I_2, I_3 assumed of the same degree, to which 3 material constants to be identified are associated, namely a, b and c . Such a function writes:

$$\Psi(\mathbf{M}, \boldsymbol{\sigma}) = aI_1(\mathbf{M}, \boldsymbol{\sigma}) + bI_2(\mathbf{M}, \boldsymbol{\sigma}) + cI_3(\mathbf{M}, \boldsymbol{\sigma}). \quad (4.2)$$

The associated strain $\boldsymbol{\epsilon}$ is given by:

$$\boldsymbol{\epsilon} = -\frac{\partial \Psi}{\partial \boldsymbol{\sigma}} = -a \frac{\partial I_1}{\partial \boldsymbol{\sigma}} - b \frac{\partial I_2}{\partial \boldsymbol{\sigma}} - c \frac{\partial I_3}{\partial \boldsymbol{\sigma}}. \quad (4.3)$$

Now assume that a linear relationship exists between invariants in the case of plane loading, Considering \mathbf{n} as a unit vector normal to the plane, the following relationship is for example obtained:

$$I_3(\mathbf{M} \cdot \mathbf{n} = 0, \boldsymbol{\sigma} \cdot \mathbf{n} = \mathbf{0}) = m I_1(\mathbf{M} \cdot \mathbf{n} = 0, \boldsymbol{\sigma} \cdot \mathbf{n} = \mathbf{0}) + n I_2(\mathbf{M} \cdot \mathbf{n} = 0, \boldsymbol{\sigma} \cdot \mathbf{n} = \mathbf{0}). \quad (4.4)$$

This means that invariants are linked by:

$$I_3(\mathbf{M}, \boldsymbol{\sigma}) = m I_1(\mathbf{M}, \boldsymbol{\sigma}) + n I_2(\mathbf{M}, \boldsymbol{\sigma}) + \mathcal{O}(\mathbf{M}, \boldsymbol{\sigma}) \quad (4.5)$$

where the function $\mathcal{O}(\mathbf{M}, \boldsymbol{\sigma})$ is written as a sum of terms in which an out-of-plane component is involved as a multiplicative factor. Thus,

$$\mathcal{O}(\mathbf{M} \cdot \mathbf{n} = 0, \boldsymbol{\sigma} \cdot \mathbf{n} = \mathbf{0}) = 0, \quad (4.6)$$

for the considered plane loading.

The strain then writes:

$$\begin{aligned} \boldsymbol{\epsilon} &= -\frac{\partial \Psi}{\partial \boldsymbol{\sigma}} = -(a + cm) \frac{\partial I_1}{\partial \boldsymbol{\sigma}} - (b + cn) \frac{\partial I_2}{\partial \boldsymbol{\sigma}} - c \frac{\partial \mathcal{O}(\mathbf{M}, \boldsymbol{\sigma})}{\partial \boldsymbol{\sigma}} \\ &= -a' \frac{\partial I_1}{\partial \boldsymbol{\sigma}} - b' \frac{\partial I_2}{\partial \boldsymbol{\sigma}} - c \frac{\partial \mathcal{O}(\mathbf{M}, \boldsymbol{\sigma})}{\partial \boldsymbol{\sigma}}. \end{aligned} \quad (4.7)$$

Its *in plane* expression simplifies into:

$$\boldsymbol{\epsilon}_{ip} = -a' \frac{\partial I_1}{\partial \boldsymbol{\sigma}_{ip}} - b' \frac{\partial I_2}{\partial \boldsymbol{\sigma}_{ip}}. \quad (4.8)$$

Out-of-plane expression gives:

$$\boldsymbol{\epsilon}_{op} = -a' \frac{\partial I_1}{\partial \boldsymbol{\sigma}_{op}} - b' \frac{\partial I_2}{\partial \boldsymbol{\sigma}_{op}} - c \frac{\partial \mathcal{O}(\mathbf{M}, \boldsymbol{\sigma})}{\partial \boldsymbol{\sigma}_{op}}. \quad (4.9)$$

It can be remarked first that the in-plane deformation involves now two constants instead of three. The expression may seem simple and the strategy which consists of a degradation of a 3D problem into a 2D problem may seem the easiest. The operation becomes much more complicated when the Gibbs free energy density involves higher degree invariants and

when in-plane and out-of-plane terms are mixed. Directly selecting a 2D integrity basis then becomes more relevant.

Note also that, although the function $\mathcal{O}(\mathbf{M}, \boldsymbol{\sigma})$ is zero for the in-plane terms, its derivative with respect to the out-of-plane terms may be not and may participate in the out-of-plane deformation. Thus, the 2D restriction of the integrity basis forbids a complete description of the out-of-plane deformation since part of the energy terms (of their derivative) is missing. **Only 2D fields are addressed with a 2D description of integrity basis.** This drawback is however of little importance since out-of-plane strain is assumed not accessible to measurement, making this part of strain tensor finally unusable. It can be noticed finally that the discussion that has been proposed for strain applies for the derivation of magnetic field too.

We now return to a more general approach. A beforehand rewriting of Ψ , involving only the invariants that cannot be rewritten when evaluated for the considered in-plane loading, as functions of some other I_k is then necessary for an efficient (low-parameter) modeling. These relations depend on the crystallographic texture of the sheet, *i.e.*, on the considered fiber (θ , α' or γ , see [Figure 2](#)).

It is obvious that the form of the stress $\boldsymbol{\sigma}$ and of the magnetization \mathbf{M} that satisfy the in-plane conditions are

$$\boldsymbol{\sigma} \cdot \mathbf{n} = 0 \quad \text{and} \quad \mathbf{M} \cdot \mathbf{n} = 0. \quad (4.10)$$

We note stress and magnetization: $\boldsymbol{\sigma}_\theta, \mathbf{M}_\theta$ (for $\mathbf{n} = \mathbf{n}_\theta$), $\boldsymbol{\sigma}_{\alpha'}, \mathbf{M}_{\alpha'}$ (for $\mathbf{n} = \mathbf{n}_{\alpha'}$) and $\boldsymbol{\sigma}_\gamma, \mathbf{M}_\gamma$ (for $\mathbf{n} = \mathbf{n}_\gamma$), for the three fibers θ , α' and γ . More precisely, the following equations describe

the in-plane hypothesis (4.10) for these three cases,

$$\boldsymbol{\sigma}_\theta = \begin{pmatrix} \sigma_{11} & \sigma_{12} & 0 \\ \sigma_{12} & \sigma_{22} & 0 \\ 0 & 0 & 0 \end{pmatrix}, \quad \mathbf{M}_\theta = \begin{pmatrix} M_1 \\ M_2 \\ 0 \end{pmatrix}, \quad (4.11)$$

$$\boldsymbol{\sigma}_{\alpha'} = \begin{pmatrix} \sigma_{11} & \sigma_{12} & -\sigma_{12} \\ \sigma_{12} & -\sigma_{23} & \sigma_{23} \\ -\sigma_{12} & \sigma_{23} & -\sigma_{23} \end{pmatrix}, \quad \mathbf{M}_{\alpha'} = \begin{pmatrix} M_1 \\ M_2 \\ -M_2 \end{pmatrix}, \quad (4.12)$$

$$\boldsymbol{\sigma}_\gamma = \begin{pmatrix} -\sigma_{12} - \sigma_{13} & \sigma_{12} & \sigma_{13} \\ \sigma_{12} & -\sigma_{12} - \sigma_{23} & \sigma_{23} \\ \sigma_{13} & \sigma_{23} & -\sigma_{13} - \sigma_{23} \end{pmatrix}, \quad \mathbf{M}_\gamma = \begin{pmatrix} M_1 \\ M_2 \\ -M_1 - M_2 \end{pmatrix}. \quad (4.13)$$

Expressions are given in the canonical cubic symmetry basis $(\mathbf{e}_1, \mathbf{e}_2, \mathbf{e}_3)$ of Figure 1, with $\mathbf{n}_\theta = \mathbf{e}_3$, $\mathbf{n}_{\alpha'} = \frac{1}{\sqrt{2}}(\mathbf{e}_2 + \mathbf{e}_3)$ and $\mathbf{n}_\gamma = \frac{1}{\sqrt{3}}(\mathbf{e}_1 + \mathbf{e}_2 + \mathbf{e}_3)$.

The assumption of plane stress leads to the reduction of the number of independent components σ_{ij} from 6 to 3. The assumption of plane magnetization reduces the number of independent components M_i to 2 instead of 3. We denote by $\mathcal{MB} = \{I_k\}$ the initial integrity basis given in Table 1. The set $\widetilde{\mathcal{MB}}$ of restrictions of polynomial functions I_k to the subspace of $(\mathbf{M}, \boldsymbol{\sigma})$ which satisfy (4.10) spans a new algebra \mathcal{A} of polynomial functions in 5 variables. Our goal is to reduce this set $\widetilde{\mathcal{MB}}$ of 30 invariants into a smaller generating set $\mathcal{G} = \{\tilde{I}_l\}$ of \mathcal{A} .

5. Reduced sets of generators for the different fibers

Several algorithms/programs, able to check whether or not a set $\mathcal{B} = \{I_j\}$ of homogeneous polynomial invariants I_j is an integrity basis, are available in the literature [20, 12, 14]. In the case of finite groups, these algorithms require the knowledge, *a priori*, of a bound on the total degree of the generators. Moreover, these algorithms also allow for reducing an integrity basis \mathcal{B} into a minimal integrity basis \mathcal{MB} , by checking linear relations among the invariants. In the present problem, a minimal integrity basis $\mathcal{MB} = \{I_k\}$ is already known and recalled in Table 1. Then, we evaluate all the I_k for a given stress/magnetization state (here for $\mathbf{M} \cdot \mathbf{n} = 0$ and $\boldsymbol{\sigma} \cdot \mathbf{n} = 0$). The restrictions of the function I_k to this subspace,

denoted by \tilde{I}_k , are however not linearly independent: they satisfy some linear relations. An algorithm to compute these relations is provided in [Appendix Appendix A](#), as well as its implementation in *Macaulay2* [21], a software system devoted to computations in algebraic geometry and commutative algebra.

Finally, a minimal set of generators $\mathcal{G} = \{\tilde{I}_{k_l}\}$ of \mathcal{A} can be produced, removing redundant generators from $\widetilde{\mathcal{MB}} = \{\tilde{I}_k\}$. This has been done for each in-plane magneto-mechanical loading (4.11), (4.12) or (4.13). Corresponding minimal sets of generators are denoted respectively by \mathcal{G}_θ , $\mathcal{G}_{\alpha'}$, and \mathcal{G}_γ . The results are summarized in [Table 3](#). The cardinalities of these sets are small (compared to the initial 30 invariants in [Table 1](#)). In terms of modeling, this means that the Gibbs free energy density can be expressed, with no lack of generality, as a function of invariants I_k such that \tilde{I}_k belongs to \mathcal{G} when in-plane stress and magnetization are considered:

$$\Psi = \Psi(I_{k_1}, \dots, I_{k_L}), \quad \tilde{I}_{k_l} \in \mathcal{G}, \quad L = \text{card } \mathcal{G}.$$

Remark 5.1. Plane constitutive laws can be deduced either by restricting first the energy density to the plane state variables and then, by deriving them with respect to these variables to get the dual plane variables (a) or by selecting the in-plane terms of 3D constitutive laws restricted to a 2D loading (b). This is mathematically justified by the fact that the *pullback* and the *exterior derivative* commute [40, theorem 5.3].

Reduced basis	Cardinal L	List of \mathbb{O} -invariants
\mathcal{G}_θ	7	$\text{tr } \boldsymbol{\sigma}, I_{002}, I_{020}, I_{200}, I_{201}, I_{210}, I_{400}$
$\mathcal{G}_{\alpha'}$	15	$\text{tr } \boldsymbol{\sigma}, I_{002}, I_{020}, I_{003}, I_{030}, I_{200}, I_{201}, I_{210}, I_{202}^a, I_{211}, I_{220}, I_{400}, I_{401}, I_{410}, I_{600}$
\mathcal{G}_γ	8	$\text{tr } \boldsymbol{\sigma}, I_{020}, I_{030}, I_{200}, I_{210}, I_{220}, I_{410}, I_{600}$

Table 3: Reduced generating sets $\mathcal{G} = \{\tilde{I}_{k_l}\}$ for the different textures.

5.1. θ -fiber

This is the most favorable texture orientation for a reduction of the integrity basis evaluated with in-plane conditions. The direction $\{001\}$ is indeed the normal $\mathbf{n}_\theta = \mathbf{e}_3$ to the cubic

crystal network (a symmetry plane of the microstructure). Because of the presence of null coefficients in (4.11) (especially on the off-diagonal part of $\boldsymbol{\sigma}$), 12 evaluated invariants in \mathcal{MB} vanish, namely

$$I_{003} = I_{004} = I_{014} = I_{202}^b = I_{203} = I_{212}^b = I_{204} = I_{402} = I_{222} = I_{401} = I_{411} = I_{600} = 0.$$

In addition, we get the following 11 relations.

$$\begin{aligned} I_{012} &= \frac{1}{6} I_{002} \operatorname{tr} \boldsymbol{\sigma}, & I_{030} &= \frac{1}{18} (9I_{020} \operatorname{tr} \boldsymbol{\sigma} - 2(\operatorname{tr} \boldsymbol{\sigma})^3), \\ I_{022} &= \frac{1}{18} (2I_{002}(\operatorname{tr} \boldsymbol{\sigma})^2 - 9I_{002}I_{020}), & I_{211} &= \frac{1}{6} I_{201} \operatorname{tr} \boldsymbol{\sigma}, \\ I_{212}^a &= \frac{1}{6} (I_{002}I_{210} - 2I_{202}^a \operatorname{tr} \boldsymbol{\sigma}), & I_{221} &= \frac{1}{18} (2I_{201}(\operatorname{tr} \boldsymbol{\sigma})^2 - 9I_{020}I_{201}), \\ I_{213} &= \frac{1}{36} I_{002}I_{201} \operatorname{tr} \boldsymbol{\sigma}, & I_{202}^a &= \frac{1}{6} I_{002}I_{200}, \\ I_{220} &= \frac{1}{18} (6I_{210} \operatorname{tr} \boldsymbol{\sigma} + 3I_{020}I_{200} - 2I_{200}(\operatorname{tr} \boldsymbol{\sigma})^2), & I_{410} &= \frac{1}{6} I_{400} \operatorname{tr} \boldsymbol{\sigma}, \\ I_{601} &= \frac{1}{18} (9I_{201}I_{400} - 4I_{200}^2I_{201}). \end{aligned}$$

5.2. α' -fiber

$\mathbf{n}_{\alpha'}$ is normal to another symmetry plane of the crystal network. This explains why the number of useful invariants is drastically reduced (this reduction is however smaller than for

the θ fiber). For this configuration, we get the following 15 relations.

$$\begin{aligned}
I_{012} &= \frac{1}{54} (-18I_{003} - 18I_{030} + 9I_{002} \operatorname{tr} \boldsymbol{\sigma} + 9I_{020} \operatorname{tr} \boldsymbol{\sigma} - 2(\operatorname{tr} \boldsymbol{\sigma})^3) \\
I_{004} &= \frac{1}{72} (9(I_{002})^2 + 6I_{002}I_{020} - 3(I_{020})^2 + 12I_{003} \operatorname{tr} \boldsymbol{\sigma} \\
&\quad - 12I_{012} \operatorname{tr} \boldsymbol{\sigma} + 12I_{030} \operatorname{tr} \boldsymbol{\sigma} - 2I_{002}(\operatorname{tr} \boldsymbol{\sigma})^2 - 2I_{020}(\operatorname{tr} \boldsymbol{\sigma})^2) \\
I_{022} &= \frac{1}{18} (-6I_{002}I_{020} + 3(I_{020})^2 - 12I_{030} \operatorname{tr} \boldsymbol{\sigma} + 2I_{020}(\operatorname{tr} \boldsymbol{\sigma})^2) \\
I_{014} &= \frac{1}{18} (6I_{020}I_{003} + 9I_{002}I_{012} + 3I_{020}I_{012} + 6I_{002}I_{030} - 2I_{002}I_{020} \operatorname{tr} \boldsymbol{\sigma} - 2I_{012}(\operatorname{tr} \boldsymbol{\sigma})^2) \\
I_{212}^a &= \frac{1}{36} (3I_{002}I_{210} - 3I_{020}I_{210} + 12I_{220} \operatorname{tr} \boldsymbol{\sigma} - 2I_{210}(\operatorname{tr} \boldsymbol{\sigma})^2) \\
I_{212}^b &= \frac{1}{36} (-9I_{002}I_{201} + 72I_{203} + 18I_{221} - 12I_{202}^b \operatorname{tr} \boldsymbol{\sigma} + 12I_{211} \operatorname{tr} \boldsymbol{\sigma} + 2I_{201}(\operatorname{tr} \boldsymbol{\sigma})^2) \\
I_{204} &= \frac{1}{18} (6I_{003}I_{210} + 9I_{002}I_{202}^a + 3I_{020}I_{202}^a + 6I_{002}I_{220} - 2I_{002}I_{210} \operatorname{tr} \boldsymbol{\sigma} - 2I_{202}^a(\operatorname{tr} \boldsymbol{\sigma})^2) \\
I_{213} &= \frac{1}{18} (3I_{003}I_{201} + 3I_{012}I_{201} - 3I_{020}I_{202}^b - 12I_{203} \operatorname{tr} \boldsymbol{\sigma} + 2I_{202}^b(\operatorname{tr} \boldsymbol{\sigma})^2) \\
I_{222} &= \frac{1}{18} (3I_{002}I_{211} - 2I_{020}I_{201} \operatorname{tr} \boldsymbol{\sigma} + 3I_{020}I_{211} + 3I_{003}I_{201} + 6I_{012}I_{201} \\
&\quad + 6I_{030}I_{201} + 2I_{202}^b(\operatorname{tr} \boldsymbol{\sigma})^2 - 2I_{211}(\operatorname{tr} \boldsymbol{\sigma})^2 - 12I_{203} \operatorname{tr} \boldsymbol{\sigma}) \\
I_{202}^b &= \frac{1}{18} (3I_{002}I_{200} + 3I_{020}I_{200} - 18I_{202}^a - 36I_{211} - 18I_{220} + 6I_{201} \operatorname{tr} \boldsymbol{\sigma} \\
&\quad + 6I_{210} \operatorname{tr} \boldsymbol{\sigma} - 2I_{200}(\operatorname{tr} \boldsymbol{\sigma})^2) \\
I_{203} &= \frac{1}{72} (12I_{003}I_{200} + 24I_{012}I_{200} + 12I_{030}I_{200} + 9I_{002}I_{201} + 3I_{020}I_{201} + 3I_{002}I_{210} - 3I_{020}I_{210} \\
&\quad - 4I_{002}I_{200} \operatorname{tr} \boldsymbol{\sigma} - 4I_{020}I_{200} \operatorname{tr} \boldsymbol{\sigma} - 12I_{202}^a \operatorname{tr} \boldsymbol{\sigma} - 24I_{211} \operatorname{tr} \boldsymbol{\sigma} + 2I_{201}(\operatorname{tr} \boldsymbol{\sigma})^2 + 2I_{210}(\operatorname{tr} \boldsymbol{\sigma})^2) \\
I_{221} &= \frac{1}{18} (-6I_{003}I_{200} - 18I_{012}I_{200} - 12I_{030}I_{200} - 6I_{020}I_{201} + 3I_{020}I_{210} + 2I_{002}I_{200} \operatorname{tr} \boldsymbol{\sigma} \\
&\quad + 4I_{020}I_{200} \operatorname{tr} \boldsymbol{\sigma} + 6I_{202}^a \operatorname{tr} \boldsymbol{\sigma} + 6I_{202}^b \operatorname{tr} \boldsymbol{\sigma} + 12I_{211} \operatorname{tr} \boldsymbol{\sigma} - 2I_{201}(\operatorname{tr} \boldsymbol{\sigma})^2 - 2I_{210}(\operatorname{tr} \boldsymbol{\sigma})^2) \\
I_{402} &= \frac{1}{72} (9I_{201}^2 + 6I_{201}I_{210} - 24I_{200}I_{211} + 3I_{020}I_{400} + 12I_{401} \operatorname{tr} \boldsymbol{\sigma} - 2I_{400}(\operatorname{tr} \boldsymbol{\sigma})^2) \\
I_{411} &= \frac{1}{144} (-9I_{201}^2 - 6I_{201}I_{210} - 24I_{200}I_{202}^b - 24I_{200}I_{211} + 12I_{002}I_{400} + 9I_{020}I_{400} \\
&\quad + 8I_{200}I_{201} \operatorname{tr} \boldsymbol{\sigma} + 12I_{401} \operatorname{tr} \boldsymbol{\sigma} - 6I_{400}(\operatorname{tr} \boldsymbol{\sigma})^2) \\
I_{601} &= \frac{1}{18} (-4I_{200}^2I_{201} + 6I_{201}I_{400} - 3I_{210}I_{400} + 6I_{200}I_{410} + I_{200}I_{400} \operatorname{tr} \boldsymbol{\sigma} - 3I_{600} \operatorname{tr} \boldsymbol{\sigma})
\end{aligned}$$

5.3. γ -fiber

In this configuration, stress tensor and magnetization do not have vanishing components (see (4.13)). However, useful relations appear between the invariants involving the off-diagonal part of $\boldsymbol{\sigma}$. We get for this fiber the following 22 relations.

$$\begin{aligned}
I_{002} &= \frac{1}{6} (12I_{020} + (\text{tr } \boldsymbol{\sigma})^2) \\
I_{012} &= \frac{1}{12} (-6I_{003} - I_{002} \text{tr } \boldsymbol{\sigma} + 9I_{020} \text{tr } \boldsymbol{\sigma}) \\
I_{003} &= \frac{1}{6} (12I_{030} - I_{002} \text{tr } \boldsymbol{\sigma} + 5I_{020} \text{tr } \boldsymbol{\sigma}) \\
I_{004} &= \frac{1}{6} (3I_{002}^2 - 18I_{002}I_{020} + 27I_{020}^2 + 2I_{003} \text{tr } \boldsymbol{\sigma}) \\
I_{022} &= \frac{1}{6} (-2I_{002}^2 + 13I_{002}I_{020} - 18I_{020}^2 - 2I_{003} \text{tr } \boldsymbol{\sigma}) \\
I_{202}^a &= \frac{1}{3} (-3I_{220} + I_{210} \text{tr } \boldsymbol{\sigma}) \\
I_{212}^a &= \frac{1}{6} (4I_{002}I_{210} - 9I_{020}I_{210} - 2I_{202}^a \text{tr } \boldsymbol{\sigma}) \\
I_{212}^b &= \frac{1}{12} (-3I_{002}I_{201} + 3I_{020}I_{201} + 12I_{203} - I_{202}^b \text{tr } \boldsymbol{\sigma} + 6I_{211} \text{tr } \boldsymbol{\sigma}) \\
I_{203} &= \frac{1}{12} (+2I_{002}I_{201} - I_{020}I_{201} - 6I_{221} - 4I_{211} \text{tr } \boldsymbol{\sigma}) \\
I_{204} &= \frac{1}{6} (2I_{003}I_{210} - 6I_{002}I_{202}^a + 18I_{020}I_{202}^a + 3I_{002}I_{210} \text{tr } \boldsymbol{\sigma} - 9I_{020}I_{210} \text{tr } \boldsymbol{\sigma}) \\
I_{213} &= \frac{1}{24} (2I_{003}I_{201} - 32I_{002}I_{211} + 72I_{020}I_{211} + 3I_{002}I_{201} \text{tr } \boldsymbol{\sigma} - 3I_{020}I_{201} \text{tr } \boldsymbol{\sigma} - 16I_{203} \text{tr } \boldsymbol{\sigma}) \\
I_{402} &= \frac{1}{36} (4I_{020}I_{200}^2 + 9I_{201}^2 - 12I_{210}^2 - 12I_{200}I_{202}^a - 3I_{002}I_{400} \\
&\quad - 6I_{020}I_{400} + 4I_{200}I_{210} \text{tr } \boldsymbol{\sigma} - 12I_{410} \text{tr } \boldsymbol{\sigma}) \\
I_{222} &= \frac{1}{54} (8I_{002}I_{201} \text{tr } \boldsymbol{\sigma} + 9I_{002}I_{202}^b - 108I_{002}I_{211} - 45I_{020}I_{202}^b + 216I_{020}I_{211} \\
&\quad + 3I_{003}I_{201} - 12I_{012}I_{201} - 36I_{203} \text{tr } \boldsymbol{\sigma}) \\
I_{014} &= \frac{1}{12} (6I_{002}I_{003} - 14I_{020}I_{003} + I_{002}^2 \text{tr } \boldsymbol{\sigma} - 6I_{002}I_{020} \text{tr } \boldsymbol{\sigma} + 9I_{020}^2 \text{tr } \boldsymbol{\sigma}) \\
I_{201} &= \frac{1}{6} (12I_{210} + I_{200} \text{tr } \boldsymbol{\sigma}) \\
I_{202}^b &= \frac{1}{6} (-4I_{002}I_{200} + 9I_{020}I_{200} - 12I_{202}^a + 3I_{201} \text{tr } \boldsymbol{\sigma}) \\
I_{211} &= \frac{1}{12} (I_{002}I_{200} + 12I_{202}^a - I_{201} \text{tr } \boldsymbol{\sigma}) \\
I_{221} &= \frac{1}{36} (-6I_{003}I_{200} - 12I_{002}I_{201} + 24I_{020}I_{201} + I_{002}I_{200} \text{tr } \boldsymbol{\sigma} + 12I_{202}^a \text{tr } \boldsymbol{\sigma}) \\
I_{400} &= \frac{1}{2} I_{200}^2 \\
I_{401} &= \frac{1}{12} (6I_{200}I_{201} - 24I_{410} - I_{200}^2 \text{tr } \boldsymbol{\sigma}) \\
I_{411} &= \frac{1}{72} (I_{002}I_{200}^2 - 6I_{201}^2 + 12I_{200}I_{202}^a + 6I_{401} \text{tr } \boldsymbol{\sigma}) \\
I_{601} &= \frac{1}{36} (I_{200}^2I_{201} - 6I_{200}I_{401} - 6I_{600} \text{tr } \boldsymbol{\sigma}) \quad 19
\end{aligned}$$

5.4. Combination of θ , α' and γ fibers

As explained in introduction of this work, it is usually possible to find a set of fibers that describes the texture of a material. If the three previous fibers are combined to form the texture of a thin layer material subjected to an in-plane magneto-mechanical loading, the invariant generators in this situation is the union of the invariant generators of each fiber. Then it can be noticed that the list of \mathbb{O} -invariants of the reduced generating sets of θ and γ fibers are included in the list of \mathbb{O} -invariants of the reduced generating set of the α' fiber. This means that the list of 15 invariants associated with the reduced generating set $\mathcal{G}_{\alpha'}$ is the reduced generating set of any combination of the three preceding fibers.

6. Application to a quadratic energy density

Let us consider a material described by a free energy density composed of three terms: a first coupled term linear in stress $\Psi_1^{\mu\sigma}(\mathbf{M}, \boldsymbol{\sigma})$, a second coupled term quadratic in stress $\Psi_2^{\mu\sigma}(\mathbf{M}, \boldsymbol{\sigma})$ and a purely magnetic term of order 6 in magnetization $\Psi^\mu(\mathbf{M})$. The purely mechanical part (quadratic in stress in the framework of linear elasticity) has no influence on magnetic field or magnetostriction, and is not considered here. A constant c_k is associated to each polynomial invariant I_k constitutive of Ψ . Thus, from the integrity basis in [Table 1](#), the free energy density writes:

$$\begin{aligned}
\Psi(\mathbf{M}, \boldsymbol{\sigma}) &= \Psi_1^{\mu\sigma}(\mathbf{M}, \boldsymbol{\sigma}) + \Psi_2^{\mu\sigma}(\mathbf{M}, \boldsymbol{\sigma}) + \Psi^\mu(\mathbf{M}) \\
&= c_{210}I_{210} + c_{201}I_{201} + c_{200,010}I_{200} \operatorname{tr}(\boldsymbol{\sigma}) \\
&\quad + c_{220}I_{220} + c_{211}I_{211} + c_{202}^a I_{202}^a + c_{202}^b I_{202}^b + c_{200,020}I_{200}I_{020} + c_{200,002}I_{200}I_{002} \quad (6.1) \\
&\quad + c_{210,010}I_{210} \operatorname{tr}(\boldsymbol{\sigma}) + c_{201,010}I_{201} \operatorname{tr}(\boldsymbol{\sigma}) + c_{200,010,010}I_{200} \operatorname{tr}(\boldsymbol{\sigma})^2 \\
&\quad + c_{200}I_{200} + c_{400}I_{400} + c_{600}I_{600}.
\end{aligned}$$

This general 3D model uses 15 material constants. In order to illustrate the reduction of this number in the case of a plane loading, we consider the following assumptions:

- the material is supplied in sheet form;
- the sheet exhibits a θ texture. Its symmetry axes coincide with those of the cubic microstructure;

- the macroscopic magnetization and stress remain in the sheet plane (2D assumption).

Following relations detailed in section 5.1, we can observe that $I_{202}^b = I_{600} = 0$. The free energy writes:

$$\begin{aligned}
\Psi_\theta &= c_{210}I_{210} + c_{201}I_{201} + c_{200,010}I_{200} \text{tr}(\boldsymbol{\sigma}) + \left(\frac{1}{3}c_{220} + c_{210,010}\right) I_{210} \text{tr}(\boldsymbol{\sigma}) \\
&+ \left(\frac{1}{6}c_{211} + c_{201,010}\right) I_{201} \text{tr}(\boldsymbol{\sigma}) + \left(\frac{1}{6}c_{220} + c_{200,020}\right) I_{200}I_{020} \\
&+ \left(\frac{1}{6}c_{202}^a + c_{200,002}\right) I_{200}I_{002} + \left(-\frac{1}{9}c_{220} + c_{200,010,010}\right) I_{200} \text{tr}(\boldsymbol{\sigma})^2 \\
&+ c_{200}I_{200} + c_{400}I_{400} + c_{211}\mathcal{O}_{211}(\mathbf{M}, \boldsymbol{\sigma}) + c_{220}\mathcal{O}_{220}(\mathbf{M}, \boldsymbol{\sigma}) + c_{202}^a\mathcal{O}_{202}^a(\mathbf{M}, \boldsymbol{\sigma}).
\end{aligned} \tag{6.2}$$

where $\mathcal{O}_k(\mathbf{M}, \boldsymbol{\sigma})$ terms are related to invariants I_k generating only out-of-plane deformations and magnetic fields. Consequently, the energy modifying the magneto-mechanical in-plane quantities simplifies (an arbitrary choice has been made on the remaining independent invariants) into:

$$\begin{aligned}
\Psi_\theta^{plane} &= c_{210}I_{210} + c_{201}I_{201} + c_{200,010}I_{200} \text{tr}(\boldsymbol{\sigma}) + c'_{210,010}I_{210} \text{tr}(\boldsymbol{\sigma}) \\
&+ c'_{201,010}I_{201} \text{tr}(\boldsymbol{\sigma}) + c'_{200,020}I_{200}I_{020} \\
&+ c'_{200,002}I_{200}I_{002} + c'_{200,010,010}I_{200} \text{tr}(\boldsymbol{\sigma})^2 \\
&+ c_{200}I_{200} + c_{400}I_{400}.
\end{aligned} \tag{6.3}$$

This formulation involves now 10 material constants instead of 15. Applying equation 4.1, the magnetostriction tensor (only relevant for 2D terms) is given by:

$$\begin{aligned}
\boldsymbol{\epsilon}^\mu &= - \left[c_{210}(\mathbf{M} \otimes \mathbf{M})^d + c_{201}(\mathbf{M} \otimes \mathbf{M})^{\bar{d}} + c'_{210,010} \left([(\mathbf{M} \otimes \mathbf{M})^d : \boldsymbol{\sigma}^d] \mathbf{1} + \text{tr}(\boldsymbol{\sigma})(\mathbf{M} \otimes \mathbf{M})^d \right) \right. \\
&+ c'_{201,010} \left([(\mathbf{M} \otimes \mathbf{M})^{\bar{d}} : \boldsymbol{\sigma}^d] \mathbf{1} + \text{tr}(\boldsymbol{\sigma})(\mathbf{M} \otimes \mathbf{M})^{\bar{d}} \right) \\
&\left. + \|\mathbf{M}\| \left(c_{200,010} \mathbf{1} + 2c'_{200,020} \boldsymbol{\sigma}^d + 2c'_{200,002} \boldsymbol{\sigma}^{\bar{d}} + 2c'_{200,010,010} \text{tr}(\boldsymbol{\sigma}) \mathbf{1} \right) \right].
\end{aligned} \tag{6.4}$$

The first two terms correspond to the usual magnetostriction terms. Those driven by constants $c'_{210,010}$ and $c'_{201,010}$ are second order magnetostriction terms. The last term is dependent on the norm of the magnetization and acts as a polarization. Note that with a constant magnetization norm, this part of the magnetostriction cannot be distinguished from the elastic deformation. The associated material constants are thus often considered to be

zero when energy is written at the magnetic domains scale [42].

Applying equation 4.1, the magnetic field (only relevant for 2D terms) is given by:

$$\begin{aligned} \mathbf{H} = & \frac{2}{\mu_0} \left(c_{200} + c_{200,010} \text{tr}(\boldsymbol{\sigma}) + c'_{200,010,010} \text{tr}(\boldsymbol{\sigma})^2 + c'_{200,020} \boldsymbol{\sigma}^d : \boldsymbol{\sigma}^d + c'_{200,002} \boldsymbol{\sigma}^{\bar{d}} : \boldsymbol{\sigma}^{\bar{d}} \right) \mathbf{M} \\ & + \frac{2}{\mu_0} \left(2c_{400} (\mathbf{M} \otimes \mathbf{M})^{\bar{d}} + c_{210} \boldsymbol{\sigma}^d + c_{201} \boldsymbol{\sigma}^{\bar{d}} + c'_{210,010} \text{tr}(\boldsymbol{\sigma}) \boldsymbol{\sigma}^d + c'_{201,010} \text{tr}(\boldsymbol{\sigma}) \boldsymbol{\sigma}^{\bar{d}} \right) \cdot \mathbf{M}. \end{aligned} \quad (6.5)$$

In many materials, magnetostriction takes place at constant volume. Applying this assumption leads to:

$$c_{200,010} = c_{210,010} = c_{201,010} = c_{200,010,010} = 0. \quad (6.6)$$

Magnetostriction expression simplifies into:

$$\begin{aligned} \boldsymbol{\epsilon}^\mu = & - \left[c_{210} (\mathbf{M} \otimes \mathbf{M})^d + c_{201} (\mathbf{M} \otimes \mathbf{M})^{\bar{d}} + \frac{1}{6} c_{211} \left([(\mathbf{M} \otimes \mathbf{M})^{\bar{d}} : \boldsymbol{\sigma}^d] \mathbf{1} + \text{tr}(\boldsymbol{\sigma}) (\mathbf{M} \otimes \mathbf{M})^{\bar{d}} \right) \right. \\ & + c_{220} \left(\left[\frac{1}{3} (\mathbf{M} \otimes \mathbf{M})^d : \boldsymbol{\sigma}^d \right] \mathbf{1} + \frac{1}{3} \text{tr}(\boldsymbol{\sigma}) (\mathbf{M} \otimes \mathbf{M})^d - \frac{2}{9} \|\mathbf{M}\| \text{tr}(\boldsymbol{\sigma}) \mathbf{1} \right) \\ & \left. + \|\mathbf{M}\| \left(2c'_{200,020} \boldsymbol{\sigma}^d + 2c'_{200,002} \boldsymbol{\sigma}^{\bar{d}} \right) \right], \end{aligned} \quad (6.7)$$

and magnetic field into:

$$\begin{aligned} \mathbf{H} = & \frac{2}{\mu_0} \left(c_{200} - \frac{1}{9} c_{220} \text{tr}(\boldsymbol{\sigma})^2 + c'_{200,020} \boldsymbol{\sigma}^d : \boldsymbol{\sigma}^d + c'_{200,002} \boldsymbol{\sigma}^{\bar{d}} : \boldsymbol{\sigma}^{\bar{d}} \right) \mathbf{M} \\ & + \frac{2}{\mu_0} \left(2c_{400} (\mathbf{M} \otimes \mathbf{M})^{\bar{d}} + c_{210} \boldsymbol{\sigma}^d + c_{201} \boldsymbol{\sigma}^{\bar{d}} + \frac{1}{3} c_{220} \text{tr}(\boldsymbol{\sigma}) \boldsymbol{\sigma}^d + \frac{1}{6} c_{211} \text{tr}(\boldsymbol{\sigma}) \boldsymbol{\sigma}^{\bar{d}} \right) \cdot \mathbf{M}. \end{aligned} \quad (6.8)$$

We can observe that strain given in equation (6.7) and strain derived from (6.1) exhibit the same in-plane components. Out-of-plane components are different as already stated. Equation (6.7) only applies for in-plane components. The linear stress part of the deformation, which is derived from the quadratic part of the free energy density, involves 5 material constants compared to 10 in the 3D model (see Table 2).

Volume conservation is a classic assumption that can be made. Using this assumption upstream in expression (6.1), the derived deformation depends on 8 parameters (7 if we take into account the fact that $I_{202}^b = 0$) against 6 in expression (6.7). Similarly, the derived magnetic field depends on 11 constants (9 if we take into account the fact that $I_{202}^b = I_{600} = 0$) against 8 in expression (6.8).

More generally, [Table 2](#) gives the number of additional coefficients depending on the degree in stress. For the same microstructure/fiber orientation, a quadratic energy density in magnetization implies 3 linear invariants in stress, 9 quadratic, 20 degree-three ... etc,. Following our method, an equivalent (for in-plane loading) energy density implies 3 linear, 5 quadratic, and 5 degree-three invariants (coming from the product of $\text{tr } \boldsymbol{\sigma}$ with 5 quadratic invariants, thanks to relations obtained in [section 5](#)). This thus leads to a quite large reduction in the number of material constants to be identified.

This reduction applies of course for other fibers: from [Table 3](#), it can be shown that a quadratic energy density involves 8 constants for a α' fiber and 5 for a γ fiber, instead of 9 in the 3D formulation. The higher the degree, the more significant the reduction.

7. Conclusion

The magneto-elasticity of cubic ferromagnetic materials is described using a Gibbs free energy density $\Psi = \Psi(I_k)$ defined as a function of well-chosen cubic invariants I_k of the stress $\boldsymbol{\sigma}$ and the magnetization \mathbf{M} . It is relevant to take these cubic invariants into account for every crystallographic texture/fiber, with the drawback that the corresponding minimal integrity basis is constituted of a quite large number (30) of invariants [[39](#), [42](#)].

The magneto-mechanical coupled behavior of textured (cubic) ferromagnetic materials subjected to in-plane magneto-mechanical loadings has been streamlined. We have shown that for such loadings, and for specific textures/fibers, the Gibbs free energy density can be written as a function of a lower number of invariants

$$\Psi = \Psi(I_{k_1}, \dots, I_{k_L}), \quad L < 30.$$

Indeed, we have computed relations among the fundamental cubic invariants I_k which arise when they are restricted to plane magneto-elasticity problems. We have obtained, this way, some reduced (minimal) sets of cardinal L of cubic generators I_{k_l} for three major fibers, namely θ ($L = 7$), α' ($L = 15$) and γ ($L = 8$) and their combination ($L = 15$). To do so, we have adapted an algorithm initially proposed to prove the minimality of an integrity basis in [[42](#)]. An implementation of this algorithm in Macaulay2, a software devoted to algebraic geometry and commutative algebra [[21](#)], has also been provided.

Appendix A. Reduction algorithm and implementation

Appendix A.1. Algorithm

The algorithm we propose here generates all the relations between the homogeneous polynomials $\{\tilde{I}_k\}$ in $\widetilde{\mathcal{MB}}$, the set of cubic invariants $\{I_k\}$ restricted to plane loadings (plane defined by the normal unit vector \mathbf{n}). For instance, for the fiber θ ($\mathbf{n}_\theta = \mathbf{e}_3$), $M_3 = 0$ and $\sigma_{13} = \sigma_{23} = \sigma_{33} = 0$. If we choose $\tilde{\mathbf{e}}_I = \mathbf{e}_1$, $\tilde{\mathbf{e}}_2 = \mathbf{e}_2$ as a natural basis of the subspace $M_3 = 0$ of vectors \mathbf{M} and

$$\tilde{\mathbf{e}}_I = \mathbf{e}_{11} = \begin{pmatrix} 1 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \end{pmatrix}, \quad \tilde{\mathbf{e}}_{II} = \mathbf{e}_{22} = \begin{pmatrix} 0 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 0 \end{pmatrix}, \quad \tilde{\mathbf{e}}_{III} = \mathbf{e}_{12} = \begin{pmatrix} 0 & 1 & 0 \\ 1 & 0 & 0 \\ 0 & 0 & 0 \end{pmatrix}$$

as a natural basis of the subspace $\boldsymbol{\sigma} \cdot \mathbf{e}_3 = 0$ of stresses $\boldsymbol{\sigma}$, we get

$$\widetilde{\mathbf{M}} = \widetilde{M}_1 \tilde{\mathbf{e}}_I + \widetilde{M}_2 \tilde{\mathbf{e}}_2 \quad \text{and} \quad \widetilde{\boldsymbol{\sigma}} = \tilde{\sigma}_1 \tilde{\mathbf{e}}_I + \tilde{\sigma}_2 \tilde{\mathbf{e}}_{II} + \tilde{\sigma}_3 \tilde{\mathbf{e}}_{III}.$$

For each considered fiber, the restricted invariants are expressed as polynomial functions of $\widetilde{\boldsymbol{\sigma}}$ and $\widetilde{\mathbf{M}}$ as above. These polynomial functions are homogeneous, both in $\widetilde{\boldsymbol{\sigma}}$ and $\widetilde{\mathbf{M}}$. For such a *bi-homogeneous polynomial*, we introduce the degree $\alpha = \deg(\widetilde{\mathbf{M}})$ in $\widetilde{\mathbf{M}}$ and the degree $\beta = \deg(\widetilde{\boldsymbol{\sigma}})$ in $\widetilde{\boldsymbol{\sigma}}$. This bi-degree is denoted by (α, β) and the total degree by $d = \alpha + \beta$. A bi-homogeneous polynomial of bi-degree (α, β) is thus a linear combination of monomials

$$m_{\boldsymbol{\alpha}, \boldsymbol{\beta}} = \widetilde{M}_1^{\alpha_1} \widetilde{M}_2^{\alpha_2} \tilde{\sigma}_1^{\beta_1} \tilde{\sigma}_2^{\beta_2} \tilde{\sigma}_3^{\beta_3} \quad (\text{A.1})$$

with $\boldsymbol{\alpha} = (\alpha_1, \alpha_2)$ (α_k being the degree in \widetilde{M}_k , so that $\alpha = |\boldsymbol{\alpha}| = \alpha_1 + \alpha_2$) and $\boldsymbol{\beta} = (\beta_1, \beta_2, \beta_3)$ (β_l being the degree in $\tilde{\sigma}_l$, so that $\beta = |\boldsymbol{\beta}| = \beta_1 + \beta_2 + \beta_3$).

On the set of bi-degrees, we introduce the *degree lexicographic order* as follows

$$(\alpha, \beta) < (\alpha', \beta') \quad \text{if} \quad \alpha + \beta < \alpha' + \beta'$$

$$\text{or} \quad \alpha + \beta = \alpha' + \beta' \quad \text{and} \quad (\alpha < \alpha' \quad \text{or} \quad \alpha = \alpha' \quad \text{and} \quad \beta < \beta').$$

Using this order relation, we define $(\alpha, \beta)_1$ and $(\alpha, \beta)_{J_{Max}}$ respectively, as the least and the greatest bi-degree (α, β) appearing in the finite list of evaluated bi-homogeneous polynomials

$\widetilde{\mathcal{MB}}$, where it is understood that each evaluated polynomial which vanishes is removed from $\widetilde{\mathcal{MB}}$. We can therefore partition $\widetilde{\mathcal{MB}}$ into bi-graded sets

$$\widetilde{\mathcal{MB}} = \widetilde{\mathcal{MB}}_{(\alpha,\beta)_1} \cup \cdots \cup \widetilde{\mathcal{MB}}_{(\alpha,\beta)_{J_{\text{Max}}}},$$

using the following partition of the integrity basis \mathcal{MB} in Table 1, and where the set $\mathcal{MB}_{\alpha,\beta}$ consists in bi-homogeneous polynomials in $(\boldsymbol{\sigma}, \mathbf{M})$ of bi-degree (α, β) .

$$\begin{aligned} \mathcal{MB}_{0,1} &= \{\text{tr } \boldsymbol{\sigma}\}, & \mathcal{MB}_{0,2} &= \{I_{020}, I_{002}\}, \\ \mathcal{MB}_{0,3} &= \{I_{012}, I_{003}, I_{030}\}, & \mathcal{MB}_{0,4} &= \{I_{004}, I_{022}\}, \\ \mathcal{MB}_{0,5} &= \{I_{014}\}, & \mathcal{MB}_{2,0} &= \{I_{200}\}, \\ \mathcal{MB}_{2,1} &= \{I_{201}, I_{210}\}, & \mathcal{MB}_{2,2} &= \{I_{202}^a, I_{202}^b, I_{211}, I_{220}\}, \\ \mathcal{MB}_{2,3} &= \{I_{210}, I_{201}\}, & \mathcal{MB}_{2,4} &= \{I_{203}, I_{212}^a, I_{212}^b, I_{221}\}, \\ \mathcal{MB}_{4,0} &= \{I_{400}\}, & \mathcal{MB}_{4,1} &= \{I_{401}, I_{410}\}, \\ \mathcal{MB}_{4,2} &= \{I_{402}, I_{411}\}, & \mathcal{MB}_{6,0} &= \{I_{600}\}, \\ \mathcal{MB}_{6,1} &= \{I_{601}\}. \end{aligned}$$

The set of all bi-homogeneous polynomials in $(\widetilde{\mathbf{M}}, \widetilde{\boldsymbol{\sigma}})$ having the same bi-degree (α, β) is a finite dimensional vector space and the subspace of such polynomials which belong to the algebra \mathcal{A} is denoted by $\mathcal{A}_{\alpha,\beta}$. Hence \mathcal{A} can be written as the direct sum

$$\mathcal{A} = \bigoplus_{\alpha,\beta} \mathcal{A}_{\alpha,\beta}.$$

Each finite dimensional vector space $\mathcal{A}_{\alpha,\beta}$ is spanned (as a vector space) by $\widetilde{\mathcal{MB}}_{\alpha,\beta}$ (which is empty if $(\alpha, \beta) > (\alpha, \beta)_{J_{\text{Max}}}$) and the so-called *reducible elements* of bi-degree (α, β) which can be written as products of (at least two) elements in

$$\bigcup_{(\mu,\nu) < (\alpha,\beta)} \widetilde{\mathcal{MB}}_{(\mu,\nu)}.$$

Hence, a minimal set of generators \mathcal{G} of \mathcal{A} can be extracted from $\widetilde{\mathcal{MB}}$ by choosing a vectorial basis in each $\mathcal{A}_{(\alpha,\beta)_J}$ ($1 \leq J \leq J_{\text{Max}}$) and by eliminating *arbitrarily* some generators \widetilde{I}_k . This can be done, bi-degree by bi-degree (α, β) , once one knows exactly the linear relations between the \widetilde{I}_k and the reducible elements of bi-degree (α, β) .

To do so, we proceed recursively as follows. Given $1 \leq J \leq J_{Max}$, let (P_1, \dots, P_N) be the N elements P_j in $\mathcal{R}_J \cup \widetilde{\mathcal{M}\mathcal{B}}_{(\alpha, \beta)_J}$, where \mathcal{R}_J is the set of reducible elements of bi-degree $(\alpha, \beta)_J$. Then, let m_1, \dots, m_M be the monomials which appear in the family of bi-homogeneous polynomials (P_1, \dots, P_N) . Each of these monomials is written $m_{(\alpha, \beta)}$ with $|\alpha| = \alpha$ and $|\beta| = \beta$ (see (A.1)). We can thus write

$$P_j = \sum_i A_{ij} m_i,$$

where $A := (A_{ij})$ is an $M \times N$ matrix. The computation of a basis $\mathbf{u}^k := \sum_i u_i^k m_i$, where $1 \leq k \leq N - R$ and $R := \text{rank}(A)$, furnishes all the independent linear relations between the P_j , which are written

$$\sum_j u_j^k P_j = 0, \quad 1 \leq k \leq N - R. \quad (\text{A.2})$$

Thanks to the knowledge of these relations, we are able to extract, *by hand*, a minimal set

$$\mathcal{G}_{(\alpha, \beta)_J} \subset \widetilde{\mathcal{M}\mathcal{B}}_{(\alpha, \beta)_J},$$

which spans (together with \mathcal{R}_J) the vector space $\mathcal{A}_{(\alpha, \beta)_J}$. The union

$$\mathcal{G} = \mathcal{G}_{(\alpha, \beta)_1} \cup \dots \cup \mathcal{G}_{(\alpha, \beta)_J} \cup \dots \cup \mathcal{G}_{(\alpha, \beta)_{J_{Max}}},$$

is then the sought minimal set of generators of the algebra \mathcal{A} .

For a given in-plane loading defined by a normal \mathbf{n} , and given by (4.10), the following algorithm produces the expected finite list of relations \mathcal{L} among the set of restricted invariants

$$\widetilde{\mathcal{M}\mathcal{B}} = \left\{ \tilde{I}_k \right\}.$$

- **Input:** The set $\widetilde{\mathcal{M}\mathcal{B}} = \left\{ \tilde{I}_k \right\}$ of restricted invariants.
- **Output:** A list $\mathcal{L}_{J_{Max}}$ of polynomials relations between these restricted invariants \tilde{I}_k .
- **Initialization:** $J = 0$, $\mathcal{L}_0 := \emptyset$.
- **For** $1 \leq J \leq J_{Max}$:
 1. Generate the family \mathcal{R}_J of all *reducible* homogeneous polynomials of bi-degree $(\alpha, \beta)_J$;

2. Compute a basis (\mathbf{u}^k) ($1 \leq k \leq N - R$) of the kernel of the matrix A ;
3. Update the list $\mathcal{L}_J := [\mathcal{L}_{J-1}, [\sum u_j^1 P_j, \dots, \sum u_j^{N-R} P_j]]$;

• **Return** $\mathcal{L}_{J_{Max}}$.

Appendix A.2. Implementation in Macaulay2

The code presented here is in the Macaulay2 language (see [21]) and can be run using a friendly web interface of Macaulay2 at

<https://www.unimelb-macaulay2.cloud.edu.au/#home>.

The invariants in Table 1 are computed for a particular form of σ and \mathbf{M} . This is the **Input** step of the algorithm detailed above. The bounds $d_{Max} = 7$ and $\alpha_{Max} = 6$ correspond respectively to the highest total degree and the highest partial degree in magnetization in the list \mathcal{MB} of invariants I_k . The increment k is associated to the total degree and α to the degree in $\tilde{\mathbf{M}}$.

```
-----Input-----
--definition of the algebra Alg of evaluated polynomials
Alg = QQ[sig1, sig2, sig3, m1, m2, Degrees=>{{0,1},{0,1},{0,1},{1,0},{1,0}}]
--off-diagonal part
dbar=(b)->(matrix{{0,b_(0,1),b_(0,2)},{b_(1,0),0,b_(1,2)},{b_(2,0),b_(2,1),0}});
--deviatoric diagonal part
ddev = (b)->(matrix{{b_(0,0) - 1/3*trace(b), 0, 0},{0, b_(1,1) -
  1/3*trace(b), 0},{0, 0, b_(2,2) - 1/3*trace(b)}});
--magnetization and stress bases for fiber theta
e1=matrix({{1_Alg},{0},{0}}); e2=matrix({{0},{1_Alg},{0}})
eI=matrix{{1_Alg,0,0},{0,0,0},{0,0,0}}
eII=matrix{{0,0,0},{0,1_Alg,0},{0,0,0}}
eIII=matrix{{0,1_Alg,0},{1_Alg,0,0},{0,0,0}}
--vectors and matrixes are omitted for others textures
--stress and magnetization for a given fiber
M = m1*e1+m2*e2
sig = sig1*eI+sig2*eII+sig3*eIII ; sigd = ddev(sig) ; sigdbar = dbar(sig)
--evaluation of the invariants
```

```

I010 = trace(sig)
I002=trace(sigdbar^2)
I020=trace(sigd*sigd)
I003=trace(sigdbar*sigdbar*sigdbar)
I012=trace(sigdbar^2*sigd)
I030=trace(sigd*sigd*sigd)
I004=trace(dbar(sigdbar^2)*dbar(sigdbar^2))
I022=trace(sigdbar*sigd*sigdbar*sigd)
I014=trace(sigdbar*dbar(sigdbar^2)*sigdbar*sigd)
I200=trace(transpose(M)*M)
I201=trace(dbar(M*transpose(M))*sigdbar)
I210=trace(ddev(M*transpose(M))*sigd)
I202a=trace(ddev(M*transpose(M))*(sigdbar^2))
I202b=trace(dbar(M*transpose(M))*dbar(sigdbar^2))
I211=trace(dbar(M*transpose(M))*sigdbar*sigd)
I220=trace((ddev(M*transpose(M)))*(sigd^2))
I203=trace(dbar(M*transpose(M))*dbar(sigdbar^2)*sigdbar)
I212a=trace(ddev(M*transpose(M))*ddev(sigdbar^2)*sigd)
I212b=trace(dbar(M*transpose(M))*dbar(sigdbar^2)*sigd)
I221=trace(dbar(M*transpose(M))*sigd*sigdbar*sigd)
I204=trace((ddev(M*transpose(M)))*sigdbar*dbar(sigdbar^2)*sigdbar)
I213=trace(dbar(M*transpose(M))*ddev(sigdbar^2)*sigdbar*sigd)
I400=trace(dbar(M*transpose(M))*dbar(M*transpose(M)))
I401=trace(dbar(M*transpose(M))*sigdbar*dbar(M*transpose(M)))
I410=trace(dbar(M*transpose(M))*sigd*dbar(M*transpose(M)))
I402=trace(dbar(M*transpose(M))*dbar(sigdbar^2)*dbar(M*transpose(M)))
I411=trace(dbar(M*transpose(M))*sigd*sigdbar*dbar(M*transpose(M)))
I600=trace(dbar(M*transpose(M))*dbar(M*transpose(M))*dbar(M*transpose(M)))
I601 = trace(ddev(M*transpose(M))*dbar(M*transpose(M))*ddev(M*transpose(M))*sigdbar)
I222=trace(dbar(M*transpose(M))*sigd*dbar(sigdbar^2)*sigd)
--creation of the list of evaluated invariants
MBtilde=new HashTable from {"I010"=>I010,"I002"=>I002,"I020"=>I020,"I003"=>I003,
"I012"=>I012,"I030"=>I030,"I004"=>I004,"I022"=>I022,"I014"=>I014,
"I200"=>I200,"I201"=>I201,"I210"=>I210,"I202a"=>I202a,"I202b"=>I202b,
"I211"=>I211,"I220"=>I220,"I203"=>I203,"I212a"=>I212a,"I212b"=>I212b,
"I221"=>I221,"I204"=>I204,"I213"=>I213,"I400"=>I400,"I401"=>I401,

```

```
"I410"=>I410,"I402"=>I402,"I411"=>I411,"I600"=>I600,"I601"=>I601,
"I222"=>I222}
```

```
--removal of vanishing invariants
```

```
MBtilde=delete(0_Alg,MBtilde)
```

```
--list of bi-degrees of MBtilde
```

```
MBtildeValues=values(MBtilde)
```

```
listDeg =apply(MBtildeValues,degree)
```

```
MBtildeIndex=keys(MBtilde)
```

```
-----
bound={7,6}
```

```
dMax=bound_0
```

```
alphaMax=bound_1
```

```
--definition of the free algebra FreeAlg
```

```
FreeAlg=QQ[MBtildeIndex,Degrees=>listDeg]
```

```
LJ={}
```

```
for k in 1..dMax do (
```

```
    for alpha in 0..alphaMax do (
```

```
        if k-alpha >= 0 then (
```

```
-----Step 1-----
```

```
            Base=toString(basis({alpha,k-alpha},FreeAlg)),
```

```
            Pj=Base,
```

```
-----Step 2-----
```

```
            for i in 0..length(MBtildeIndex)-1 do (
```

```
                Pj=replace(toString(MBtildeIndex_i),concatenate("
```

```
                (",(toString(MBtildeValues_i)),")"),Pj)
```

```
            ),
```

```
            Pj=value Pj,
```

```
            if Pj!=0_Alg then (
```

```
                mi=monomials(Pj),
```

```
                (m,A)=coefficients(Pj,Monomials=>mi),
```

```
                uj=generators(ker A),
```

```
-----Step 3-----
```

```
                ujPj=(value(Base))*value(toString(uj)),
```

```
                if ujPj!=0 then (
```

```
                    LJ=append(LJ,ujPj)) ,
```

```
            )
```

```
)
)
)
"LJMax"<<toString(LJ)<<close
```

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